# **APPENDICIES**

# Appendix 1: Abbreviation Key for Mass-Volume Model

| Abbreviation  |  |  |  |  |
|---|--|--|--|--|
| Kf sd = associated rate constant for stomach and duodenum |  |  |  |  |
| Ka dj = associated rate constant for duodenum and jejunum |  |  |  |  |
| Ka ji = associated rate constant for jejunum and ileum    |  |  |  |  |
| Ka ie = associated rate constant for ileum and colon      |  |  |  |  |
| Ka co = associated rate constant for colon and excretion  |  |  |  |  |
| SD trans = transfer rate between stomach and duodenum     |  |  |  |  |
| DJ trans = transfer rate between duodenum and jejunum     |  |  |  |  |
| JL trans = transfer rate between jejunum and ileum        |  |  |  |  |
| IC trans = transfer rate between ileum and colon          |  |  |  |  |
| Waste = transfer rate between colon and excretion         |  |  |  |  |
| pH s = pH stomach   |  |  |  |  |
| pH s2 = pH duodenum                                       |  |  |  |  |
| pH s3 = pH jejunum  |  |  |  |  |
| pH s4 = pH ileum  |  |  |  |  |
| pH s5 = pH colon  |  |  |  |  |
| sol profile = solubility profile for stomach              |  |  |  |  |

| sol profile 2 = solubility profile for duodenum                     |  |  |  |  |  |
|---|--|--|--|--|--|
| sol profile 3 = solubility profile for jejunum                      |  |  |  |  |  |
| sol profile 4 = solubility profile for ileum                        |  |  |  |  |  |
| sol profile 5 = solubility profile for colon                        |  |  |  |  |  |
| stom ka = associated rate constant for stomach compartments 1 and 2 |  |  |  |  |  |
| duo ka = associated rate constant for duodenum compartments 1 and 2 |  |  |  |  |  |
| Jej ka = associated rate constant for jejunum compartments 1 and 2  |  |  |  |  |  |
| Il ka = associated rate constant for ileum compartments 1 and 2     |  |  |  |  |  |
| Colon ka = associated rate constant for colon compartments 1 and 2  |  |  |  |  |  |
| SA stom = surface area of stomach                                   |  |  |  |  |  |
| SA duo = surface area of duodenum                                   |  |  |  |  |  |
| SA jej = surface area of jejunum                                    |  |  |  |  |  |
| SA il = surface area of ileum                                       |  |  |  |  |  |
| SA colon = surface area of colon                                    |  |  |  |  |  |
| Perm stom = permeability of stomach                                 |  |  |  |  |  |
| Perm duo = permeability of duodenum                                 |  |  |  |  |  |
| Perm jej = permeability of jejunum                                  |  |  |  |  |  |
| Perm il = permeability of ileum                                     |  |  |  |  |  |
| Perm colon = permeability of colon                                  |  |  |  |  |  |

Ka sd = associated rate construct for stomach fluid absorption

Ka du = associated rate construct for duodeunm fluid absorption

Ka je = associated rate construct for jejunm fluid absorption

Ka il = associated rate construct for ileunm fluid absorption

Ka co = associated rate construct for colon fluid absorption

Note: other abbreviations adhere to above descriptors and are self explanatory

# Appendix 2: Equations, Parameters and Values For Mass-Volume Model

```
amt_plasma(t) = amt_plasma(t - dt) + (trans_21 + ka - elimination - trans_12) * dt
 INIT amt plasma = 0
 INFLOWS:
 trans_21 = k21*comp 2
 ka = tot abs rate
 OUTFLOWS:
 elimination = amt plasma*k elim
 trans_12 = k12*amt plasma
 blood_side_col(t) = blood_side_col(t - dt) + (colon_ka_5) * dt
 INIT blood side col = 0
INFLOWS:
colon_ka_5 = IF Vol_colon*sol_profile_5 >=Colon THEN Colon*SA_colon*perm_colon*3600
ELSE Vol_colon*sol_profile_5*SA_colon*perm_colon*3600
blood\_side\_dou(t) = blood\_side\_dou(t - dt) + (duo\_ka) * dt
INIT blood side dou = 0
INFLOWS:
duo ka
                     IF
                             Vol duod*sol profile 2
                                                                                   THEN
duodenum*SA_duo*perm_duo*3600 ELSE Vol_duod*sol_profile_2*SA_duo*perm_duo*3600
blood\_side\_il(t) = blood\_side\_il(t - dt) + (Il\_ka) * dt
INIT blood side il = 0
INFLOWS:
Il_ka = IF Vol_ileum*sol_profile_4 >=Ileum THEN Ileum*SA_II*perm_II*3600
                                                                                   ELSE
Vol_ileum*sol_profile_4*SA_Il*perm_Il*3600
blood\_side\_jej(t) = blood\_side\_jej(t - dt) + (Jej\_ka) * dt
INIT blood_side_jej = 0
INFLOWS:
Jej_ka = IF Vol_jej*sol_profile_3 >=Jejunum THEN Jejunum*SA_jej*perm_jej *3600 ELSE
Vol_jej*sol_profile_3*SA_jej*perm_jej*3600
blood\_side\_sto(t) = blood\_side\_sto(t - dt) + (stom ka) * dt
INIT blood side sto = 0
INFLOWS:
stom_ka = IF Vol_stom*sol_profile >= Stomach THEN Stomach*SA_stom*perm_stom*3600
ELSE Vol_stom*sol_profile*SA stom*perm_stom*3600
Colon(t) = Colon(t - dt) + (IC_{trans} - Waste - colon ka 5) * dt
INIT Colon = 0
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INFLOWS:
IC_trans = ka_ic*Ileum
OUTFLOWS:
 Waste = ka col*Colon
colon_ka_5 = IF Vol_colon*sol_profile_5 >=Colon THEN Colon*SA_colon*perm_colon*3600
ELSE Vol_colon*sol_profile_5*SA_colon*perm_colon*3600
comp_2(t) = comp_2(t - dt) + (trans_12 - trans_21) * dt
INIT comp 2 = 0
INFLOWS:
trans 12 = k12*amt plasma
OUTFLOWS:
trans_21 = k21*comp 2
duodenum(t) = duodenum(t - dt) + (SD_trans - duo ka - DJ trans) * dt
INIT duodenum = 0
INFLOWS:
SD_trans = if Stomach > 0 then kf sd*Stomach else 0
OUTFLOWS:
                    IF
                            Vol duod*sol profile 2
                                                                  duodenum
                                                                                 THEN
duodenum*SA_duo*perm_duo*3600 ELSE Vol_duod*sol_profile_2*SA_duo*perm_duo*3600
DJ_trans = ka dj*duodenum
excretion(t) = excretion(t - dt) + (vol cw) * dt
INIT excretion = 0
INFLOWS:
vol_cw = Vol_colon*ka col
excretion_2(t) = excretion 2(t - dt) + (Waste) * dt
INIT excretion 2 = 0
INFLOWS:
Waste = ka col*Colon
Ileum(t) = Ileum(t - dt) + (JL trans - IC trans - Il ka) * dt
INIT Ileum = 0
INFLOWS:
JL_trans = ka_ji*Jejunum
OUTFLOWS:
IC_trans = ka ic*Ileum
Il_ka = IF Vol_ileum*sol_profile_4 >= Ileum THEN Ileum*SA_Il*perm_II*3600
                                                                                 ELSE
Vol_ileum*sol_profile_4*SA_Il*perm_Il*3600
Jejunum(t) = Jejunum(t - dt) + (DJ trans - JL trans - Jej ka) * dt
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INIT Jejunum = 0
 INFLOWS:
 DJ_trans = ka_dj*duodenum
 OUTFLOWS:
 JL_trans = ka ji*Jejunum
Jej_ka = IF Vol_jej*sol_profile_3 >=Jejunum THEN Jejunum*SA_jej*perm_jej *3600 ELSE
 Vol_jej*sol_profile_3*SA_jej*perm_jej*3600
serosal_col(t) = serosal_col(t - dt) + (Adsorp_col - col_secretion) * dt
 INIT serosal col = 0
INFLOWS:
Adsorp\_col = PULSE(1.67,0,.1) + 0*Vol\_colon*ka\_co
OUTFLOWS:
col_secretion = 0
serosal\_dou(t) = serosal\_dou(t - dt) + (Adsorp\_Duo - duo\_secretion) * dt
INIT serosal dou = 0
INFLOWS:
Adsorp\_Duo = PULSE(10.82,0,.1) + 0*Vol\_duod*ka du
OUTFLOWS:
duo_secretion = PULSE(10.82,0.1)
serosal_ill(t) = serosal_ill(t - dt) + (Adsorpt_ill - ile_secretion) * dt
INIT serosal ill = 0
INFLOWS:
Adsorpt_ill = PULSE(8.83,0,.10)+0*Vol_ileum*ka il
OUTFLOWS:
ile_secretion = PULSE(1.50,0.1)
serosal_jej(t) = serosal_jej(t - dt) + (Adsorp_jej - jej_secretion) * dt
INIT serosal jej = 0
INFLOWS:
Adsorp\_jej = PULSE(15.76,0,.1) + 0*Vol\_jej*ka\_je
OUTFLOWS:
jej secretion = PULSE(2.67,0..1)
serosal\_sto(t) = serosal\_sto(t - dt) + (Adsorp\_Stom - Stom\_Secretion) * dt
INIT serosal_sto = 0
INFLOWS:
Adsorp_Stom = 0*Vol stom*ka sd
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OUTFLOWS:
          Stom Secretion = PULSE(16.67,0,.1)
          Stomach(t) = Stomach(t - dt) + (-SD_trans - stom_ka) * dt
          INIT Stomach = 1000
          OUTFLOWS:
          SD_trans = if Stomach > 0 then kf sd*Stomach else 0
          stom_ka = IF Vol_stom*sol_profile >= Stomach THEN Stomach*SA_stom*perm_stom*3600
          ELSE Vol_stom*sol_profile*SA stom*perm stom*3600
          total_drug_absorbed(t) = total_drug_absorbed(t - dt) + (tot abs_rate) * dt
          INIT total drug absorbed = 0
          INFLOWS:
          tot_abs_rate = stom_ka+duo_ka+Jej_ka+Il_ka+colon ka 5
          Total Elimination(t) = Total Elimination(t - dt) + (elimination) * dt
          INIT Total Elimination = 0
         INFLOWS:
          elimination = amt plasma*k elim
          Vol_{colon(t)} = Vol_{colon(t - dt)} + (vol_{ij} + col_{secretion} - vol_{cw} - Adsorp_{col}) * dt
         INIT Vol_colon = 0
         INFLOWS:
         vol_ij = Vol_ileum*ka ic
OUTFLOWS:
vol cw = Vol colon*ka col
Adsorp_col = PULSE(1.67,0,1)+0*Vol colon*ka co
Vol_duod(t) = Vol_duod(t - dt) + (vol_sd + duo_secretion - voil_dj - Adsorp_Duo) * dt
          INIT Vol. duod = 0
          INFLOWS:
          vol_sd = kf_sd*Vol_stom
          duo secretion = PULSE(10.82,0,1)
          OUTFLOWS:
          voil_dj = Vol_duod*ka_dj
          Adsorp_Duo = PULSE(10.82,0,.1) + 0*Vol_duod*ka_du
          Vol ileum(t) = Vol ileum(t - dt) + (vol ji + ile secretion - Adsorpt ill - vol ij) * dt
          INIT Vol ileum = 0
          INFLOWS:
          vol_ji = Vol_jej*ka_ji
          ile_secretion = PULSE(1.50,0,1)
```

```
OUTFLOWS:
    Adsorpt_ill = PULSE(8.83,0,.10)+0*Vol_ileum*ka_il
    vol ij = Vol_ileum*ka_ic
    Vol jej(t) = Vol jej(t - dt) + (voil dj + jej secretion - vol ji - Adsorp jej) * dt
    INIT Vol jej = 0
    INFLOWS:
    voil dj = Vol duod*ka dj
    jej secretion = PULSE(2.67,0,1)
    OUTFLOWS:
    vol ji = Vol jej*ka ji
    Adsorp jej = PULSE(15.76,0,1)+0*Vol jej*ka_je
    Vol stom(t) = Vol stom(t - dt) + (Stom Secretion - vol sd - Adsorp Stom) * dt
    INIT Vol stom = PULSE(8.33,0,1)
   INFLOWS:
   Stom_Secretion = PULSE(16.67,0,.1)
OUTFLOWS:
\sqrt{2} vol_sd = kf_sd*Vol_stom
    Adsorp\_Stom = 0*Vol\_stom*ka sd
   conc plasma = (amt plasma/volume)*mg to ug
4 k12 = .839
   k21 = .67
    ka co = 1
    ka col = 3
    ka di = 3
    ka du = 1
    ka_ic = 3
    ka il = 8.83
    ka je = 1
    ka ji = 3
    ka sd = 1
    kf sd = 2.8
    k = .161
    mg_{to}ug = 1000
    perm colon = 3.80e-6
    perm_duo = 1.10e-6
    perm Il = 4.06e-6
    perm_{jej} = 2.17e-6
    perm stom = 1.10e-6
    ph s = 1.5
    ph_s_2 = 6.6
    ph_s_3 = 6.6
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ph s 4 = 7.5
ph s 5 = 6.6
 SA colon = 138
 SA duo = 125
SA Il = 102
SA \text{ jej} = 182
SA stom = 50
volume = 4*19200
sol profile = GRAPH(ph s)
(1.00, 63.0), (1.50, 25.0), (2.00, 10.0), (2.50, 5.00), (3.00, 4.00), (3.50, 3.80), (4.00, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), 
3.50), (5.00, 3.65), (5.50, 3.65), (6.00, 3.65), (6.50, 3.65), (7.00, 3.65), (7.50, 3.65), (8.00, 3.65),
(8.50, 4.00), (9.00, 5.00), (9.50, 12.0), (10.0, 23.5)
sol profile 2 = GRAPH(ph s 2)
(1.00, 63.0), (1.50, 25.0), (2.00, 10.0), (2.50, 5.00), (3.00, 4.00), (3.50, 3.80), (4.00, 3.65), (4.50, 3.60), (4.00, 3.65), (4.50, 3.60), (4.00, 3.65), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), (4.50, 3.60), 
3.50), (5.00, 3.65), (5.50, 3.65), (6.00, 3.65), (6.50, 3.65), (7.00, 3.65), (7.50, 3.65), (8.00, 3.65),
(8.50, 4.00), (9.00, 5.00), (9.50, 12.0), (10.0, 23.5)
sol profile 3 = GRAPH(ph s 3)
(1.00, 63.0), (1.50, 25.0), (2.00, 10.0), (2.50, 5.00), (3.00, 4.00), (3.50, 3.80), (4.00, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), 
3.50), (5.00, 3.65), (5.50, 3.65), (6.00, 3.65), (6.50, 3.65), (7.00, 3.65), (7.50, 3.65), (8.00, 3.65),
(8.50, 4.00), (9.00, 5.00), (9.50, 12.0), (10.0, 23.5)
sol_profile 4 = GRAPH(ph s 4)
(1.00, 63.0), (1.50, 25.0), (2.00, 10.0), (2.50, 5.00), (3.00, 4.00), (3.50, 3.80), (4.00, 3.65), (4.50, 3.65)
3.50), (5.00, 3.65), (5.50, 3.65), (6.00, 3.65), (6.50, 3.65), (7.00, 3.65), (7.50, 3.65), (8.00, 3.65),
(8.50, 4.00), (9.00, 5.00), (9.50, 12.0), (10.0, 23.5)
sol profile 5 = GRAPH(ph s 5)
(1.00, 63.0), (1.50, 25.0), (2.00, 10.0), (2.50, 5.00), (3.00, 4.00), (3.50, 3.80), (4.00, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), 
 3.50), (5.00, 3.65), (5.50, 3.65), (6.00, 3.65), (6.50, 3.65), (7.00, 3.65), (7.50, 3.65), (8.00, 3.65),
(8.50, 4.00), (9.00, 5.00), (9.50, 12.0), (10.0, 23.5)
```

#### Appendix 3: Abbreviation Key For GI Model

The legend/key has been divided into sub-sections corresponding to the sub-sections of the model diagram.

Numbered suffixes (1, 2, 3, 4, 5, 6) have been assigned to distinguish between intestinal regions (stomach, duodenum, jejunum, ileum, colon, and waste, respectively).

- 1 stomach
- 2 duodenum
- 3 jejunum
- 4 ileum
- 5 colon
- 6 waste

For example, VOL 1 is the volume in the stomach, MASS 3 is the insoluble mass in the jejunum. In the equations, COMP 1 indicates the stomach, COMP 2 the duodenum, COMP 3, the jejunum, etc.

Ghosts are listed under the sub-section containing the original reservoir, flow regulator, or converter.

Abbreviations listed in italics are regionally dependent and set up as arrays to allow independent values for each intestinal region.

In general, ADJ as a prefix indicates a calculated parameter value (ADJ = adjusted), while ADJ as a suffix indicates an adjustment parameter (ADJ = adjustment).

### Intestinal model

#### Reservoirs/Compartments

VOL ABS Fluid volume absorbed VOL Fluid volume

C REL Mass of drug contained with a formulation or controlled release

device

MASS Insoluble mass of drug (not contained within the formulation or

controlled release device)

SOL Soluble mass of drug

ABSORPTION Mass of drug absorbed

Flow regulators

REABS Rate of water absorption VOL OUT Fluid volume transit rate

CR OUT Formulation or controlled release device transit rate

CR INPUT Drug release rate from formulation or controlled release device

MASS OUT Insoluble drug mass transit rate

DISS PRECIP Dissolution rate

SOL OUT Soluble drug mass transit rate

FLUX Absorption rate

### ADJ PARMS (Adjustment Parameters)

VOL ADJ Fluid volume absorption adjustment parameter

DISS ADJ Dissolution rate adjustment parameter
TRANSIT ADJ Transit time adjustment parameter
SA ADJ Surface area adjustment parameter

FLUX ADJ Passive Absorption adjustment parameter EFFLUX ADJ Efflux or secretion adjustment parameter CARRIER ADJ Active absorption adjustment parameter

## PARMS (Parameters)

VOL PARM Fluid volume absorption rate constant SURFACE AREA Surface area available for absorption

DOSE The administered dose of drug

INIT VOLUME The administered volume of water or fluid

TIME IN HOURS A clock

pH The physiological pH value

PARACELLULAR A user controlled switch used to adjust absorption based on

absorption mechanism

#### TRANSIT TIME

TRANSFERS GI transit rate constant
CUMU TT Cumulative transit time

ADJ TRANSIT TIME Adjusted GI transit time incorporating adjustment parameter and

user input

USER TT INPUT

User controlled adjustments to the GI transit time

#### **OUTPUT CALCULATIONS**

ABSORBED TOTAL Total mass of drug absorbed (sum of ABSORPTION 1...5)

 FDp% Fraction or the dose absorbed into portal vein x 100

**FLUX TOTAL** Total absorption rate (sum of FLUX 1...5)

**CUM DISS** Cumulative drug mass dissolved

CR Release Cumulative drug mass released from formulation

**CUM DISS RATE** Sum of DISS PRECIP 1...5 CR cumrate Summ of CR INPUT 1...5

#### PERMEABILITY CALCULATION

ADJ PERM Adjusted permeability ncorporating all transport mechanisms and

relevant adjustment parameters

ACT PE Active or carrier-mediated absorptive permeability

Constant from the Michaelis-Mentin type permeability equation for Km

active transport

**REGIONAL** Passive permeability after regional correlation calculation (same as

PASS PE if regional correlation is not used)

PASS PE Passive permeability entered by user

RC A logical function used in determining the regional correlation **RCSUM** A logical function used in determining the regional correlation

## SOLUBILITY CALCULATION

USER pH User supplied pH value for which a solubility value is available

USER SOLUB User supplied solubility value corresponding to the USER pH value ADJ SOLUB

Solubility calculated (if necessary) at the appropriate pH value

using the entered USER pH and USER SOLUB values

## CONTROLLED RELEASE CALCULATION

CR RATE The instantaneous release rate from the formulation

CR DOSE The total dose contained with the formulation

CR AT TIME The cumulative drug mass release profile

CR AT LAST The cumulative drug mass release profile

Note: CR AT TIME holds the value at the current time value (t), CR AT LAST holds the value at the immediately preceeding time value (t-1)

#### CONC CALCULATION

CONCENTRATIONS The dissolved drug concentration

## DISSOLUTION CALCULATION

**PRECIP** DISSOL Precipitation rate constant Dissolution rate constant

ADJ DISS PRECIP

Adjusted rate constant incorporating PRECIP, DISSOL and calculated concentration

Appendix 4: Equations, Parameters and Values For GI Model

```
ADJ PARMS
          CARRIER_ADJ[COMPS] = 0
DISS_ADJ[COMP_1] = 1
DISS_ADJ[COMP_2] = 1
DISS_ADJ[COMP_3] = 1
DISS_ADJ[COMP_4] = 1
DISS_ADJ[COMP_5] = 1
EFFLUX_ADJ[COMPS] = 1
FLUX_ADJ[COMP_1] = 1
FLUX_ADJ[COMP_2] = 10
FLUX_ADJ[COMP_3] = 8
FLUX_ADJ[COMP_4] = 2
FLUX_ADJ[COMP_5] = 1
SA_ADJ[COMP_1] = 1
SA_ADJ[COMP_1] = 1
SA_ADJ[COMP_1] = 1
SA_ADJ[COMP_2] = 1
SA_ADJ[COMP_3] = 1
TRANSIT_ADJ[COMP_1] = 1
            CARRIER_ADJ[COMPS] = 0
 5
10
 TRANSIT ADJ[COMP 1] = 1
               TRANSIT_ADJ[COMP_2] = 1
              TRANSIT_ADJ[COMP_3] = 1
 TRANSIT ADJ[COMP 4] = 1
               TRANSIT_ADJ[COMP_5] = 1
 <u>إشا</u>
              VOL_ADJ[COMP_1] = 1
               VOL ADJ[COMP 2] = 1
 Ŋ
               VOL\_ADJ[COMP\_3] = 1
               VOL\_ADJ[COMP\_4] = 1
 VOL_ADJ[COMP_5] = 1
       CONC CALCULATION
           ○ CONCENTRATIONS[COMP_1] = if VOL_1=0.0 then 0 else if
                ADJ_SOLUB[COMP_1]<SOL_1/VOL_1 then ADJ_SOLUB[COMP_1] else SOL_1/VOL_1 +
                0°(SOL 2+SOL 5+SOL 3+SOL 4+VOL 3+VOL_2+VOL_4+VOL_5)
           CONCENTRATIONS[COMP_2] = if VOL_2 = 0.0 then 0 else if (VOL_2<1e-6 AND SOL_2<1e-7)
                then 0 else if ADJ_SOLUB[COMP_2]<SOL_2/VOL_2 then ADJ_SOLUB[COMP_2] else
                SOL 2NOL 2
                +0*(SOL_1+SOL_5+SOL_3+SOL_4+VOL_3+VOL_1+VOL_5+VOL_4)
           CONCENTRATIONS[COMP_3] = if VOL_3 = 0.0 then 0 else if (VOL_3<1e-6 AND SOL_3<1e-7)
                then 0 else if ADJ_SOLUB[COMP_3]<SOL_3/VOL_3 then ADJ_SOLUB[COMP_3] else
                SOL 3/VOL_3
                +0*(SOL_1+SOL_2+SOL_4+SOL_5+VOL_5+VOL_4+VOL_1+VOL_2)
           CONCENTRATIONS[COMP_4] = if VOL_4 = 0.0 then 0 else if (VOL_4<1e-6 AND SOL_4<1e-7)
                then 0 else if ADJ_SOLUB[COMP_4]<SOL_4/VOL_4 then ADJ_SOLUB[COMP_4] else
                SOL 4/VOL_4
                +0*(SOL 1+SOL 2+SOL 3+SOL_5+VOL_1+VOL_2+VOL_3+VOL_5)
```

- CONCENTRATIONS[COMP\_5] = if VOL\_5 = 0.0 then 0 else if (VOL\_5<1e-6 AND SOL\_5<1e-7) then 0 else if ADJ\_SOLUB[COMP\_5]<SOL\_5/VOL\_5 then ADJ\_SOLUB[COMP\_5] else SOL 5/VOL\_5 +0\*(SOL\_1+SOL\_4+SOL\_3+SOL\_2+VOL\_3+VOL\_1+VOL\_2+VOL\_4) CONTROL RELEASE CALCULATION CR DOSE = 0
- CR\_RATE = (CR\_AT\_TIME-CR\_AT\_LAST)\*20\*(CR\_DOSE/100)
- CR AT LAST = GRAPH(TIME-DT) (0.00, 0.00), (0.25, 17.7), (0.5, 31.5), (0.75, 42.2), (1.00, 50.6), (1.25, 57.1), (1.50, 62.1), (1.75, 62.1), (66 1), (2.00, 69.2), (2.25, 71.6), (2.50, 73.4), (2.75, 74.9), (3.00, 76.0), (3.25, 76.9), (3.50, 77.6), (3.75, 78.1), (4.00, 78.5), (4.25, 78.9), (4.50, 79.1), (4.75, 79.3), (5.00, 79.5), (5.25, 79.6), (5.50, 79.6),79.7), (5.75, 79.7), (6.00, 79.8), (6.25, 79.8), (6.50, 79.9), (6.75, 79.9), (7.00, 79.9), (7.25, 79.9), (7.50, 80.0), (7.75, 80.0), (8.00, 80.0), (8.25, 80.0), (8.50, 80.0), (8.75, 80.0), (9.00, 80.0), (9.25, 80.0), (9.00, 80.0),80 0), (9.50, 80.0), (9.75, 80.0), (10.0, 80.0), (10.3, 80.0), (10.5, 80.0), (10.8, 80.0), (11.0, 80.0), (11.3, 80.0), (11.5, 80.0), (11.8, 80.0), (12.0, 80.0), (12.3, 80.0), (12.5, 80.0), (12.8, 80.0), (13.0, 80.0)...
- CR\_AT\_TIME = GRAPH(TIME) (0.00, 0.00), (0.25, 17.7), (0.5, 31.5), (0.75, 42.2), (1.00, 50.6), (1.25, 57.1), (1.50, 62.1), (1.75, 1.50, 1.66.1), (2.00, 69.2), (2.25, 71.6), (2.50, 73.4), (2.75, 74.9), (3.00, 76.0), (3.25, 76.9), (3.50, 77.6), (3.75, 78.1), (4.00, 78.5), (4.25, 78.9), (4.50, 79.1), (4.75, 79.3), (5.00, 79.5), (5.25, 79.6), (5.50, 79.6),79.7), (5.75, 79.7), (6.00, 79.8), (6.25, 79.8), (6.50, 79.9), (6.75, 79.9), (7.00, 79.9), (7.25, 79.9), (7.50, 80.0), (7.75, 80.0), (8.00, 80.0), (8.25, 80.0), (8.50, 80.0), (8.75, 80.0), (9.00, 80.0), (9.25, 80.0), (9.00, 80.0),80.0), (9.50, 80.0), (9.75, 80.0), (10.0, 80.0), (10.3, 80.0), (10.5, 80.0), (10.8, 80.0), (11.0, 80.0), (11.3, 80.0), (11.5, 80.0), (11.8, 80.0), (12.0, 80.0), (12.3, 80.0), (12.5, 80.0), (12.8, 80.0), (13.0, 80.0)...

#### DISSOLUTION CALCULATION

- ADJ\_DISS\_PRECIP[COMP\_1] = if VOL\_1=0 then 0 else if (SOL 1/VOL\_1<ADJ\_SOLUB[COMP\_1]) then (DISSOL[COMP\_1]\*DISS\_ADJ[COMP\_1]\*MASS\_1\*(ADJ\_SOLUB[COMP\_1]-SOL\_1/VOL\_1)) else ((SOL\_1/VOL\_1)-ADJ\_SOLUB[COMP\_1])\*PRECIP[COMP\_1]+ 0\*(MASS 1+MASS 2+MASS\_3+MASS\_4+MASS\_5+SOL\_1+SOL\_2+SOL\_3+SOL\_4+SOL\_5+V OL 1+VOL 2+VOL\_3+VOL\_4+VOL\_5)
- ADJ\_DISS\_PRECIP[COMP\_2] = if VOL\_2=0 then 0 else if (SOL 2/VOL 2<ADJ SOLUB[COMP\_2]) then (DISSOLICOMP 2]\*DISS\_ADJ[COMP\_2]\*MASS\_2\*(ADJ\_SOLUB[COMP\_2]-SOL\_2/VOL\_2)) else ((SOL\_2/VOL\_2)-ADJ\_SOLUB[COMP\_2])\*PRECIP[COMP\_2] +0\*(MASS\_1+MASS\_2+MASS\_3+MASS\_4+MASS\_5+SOL\_1+SOL\_2+SOL\_3+SOL\_4+SOL\_5+V OL\_1+VOL\_2+VOL\_3+VOL\_4+VOL\_5)
- ADJ\_DISS\_PRECIP[COMP\_3] = if VOL\_3=0 then 0 else if (SOL\_3/VOL\_3<ADJ\_SOLUB[COMP\_3]) then (DISSOL[COMP\_3]\*DISS\_ADJ[COMP\_3]\*MASS\_3\*(ADJ\_SOLUB[COMP\_3]-SOL\_3/VOL\_3)) else ((SOL\_3/VOL\_3)-ADJ\_SOLUB[COMP\_3])\*PRECIP[COMP\_3] +0\*(MASS\_1+MASS\_2+MASS\_3+MASS\_4+MASS\_5+SOL\_1+SOL\_2+SOL\_3+SOL\_4+SOL\_5+V OL 1+VOL 2+VOL 3+VOL 4+VOL\_5)

```
ADJ_DISS_PRECIP[COMP_4] = if VOL_4=0 then 0 else if
       (SOL 4/VOL_4<ADJ_SOLUB[COMP 4]) then
       (DISSOL[COMP_4]*DISS_ADJ[COMP_4]*MASS_4*(ADJ_SOLUB[COMP_4]-SOL_4/VOL_4)) else
       ((SOL 4NOL 4)-ADJ SOLUB[COMP 4])*PRECIP[COMP 4]
       +0*(MASS_1+MASS_2+MASS_3+MASS_4+MASS_5+SOL_1+SOL_2+SOL_3+SOL_4+SOL_5+V
       OL 1+VOL 2+VOL 3+VOL 4+VOL 5)
   ADJ_DISS_PRECIP[COMP_5] = if VOL_5=0 then 0 else if
       (SOL_5/VOL_5<ADJ_SOLUB[COMP_5]) then
       (DISSOL[COMP_5]*DISS_ADJ[COMP_5]*MASS_5*(ADJ_SOLUB[COMP_5]-SOL_5/VOL_5)) else
       ((SOL 5/VOL 5)-ADJ_SOLUB[COMP_5])*PRECIP[COMP_5]
       +0*(MASS_1+MASS_2+MASS_3+MASS_4+MASS_5+SOL_1+SOL_2+SOL_3+SOL_4+SOL_5+V
  OL_1+VOL_2+VOL_3+\
DISSOL[COMP_1] = 1
DISSOL[COMP_2] = 1
DISSOL[COMP_3] = 1
DISSOL[COMP_4] = 1
DISSOL[COMP_5] = 1
PRECIP[COMP_1] = 10
PRECIP[COMP_2] = 10
PRECIP[COMP_3] = 10
PRECIP[COMP_4] = 10
       OL 1+VOL_2+VOL_3+VOL_4+VOL_5)
PRECIP[COMP 4] = 10
     PRECIP[COMP 5] = 10
    INPUTS
    INTESTINAL MODEL
       ABSORPTION_1(t) = ABSORPTION_1(t - dt) + (FLUX_1) * dt
       INIT ABSORPTION 1 = 0
        INFLOWS:
TU
          ★ FLUX_1 =
<u>ا</u>
              CONCENTRATIONS[COMP_1]*ADJ_PERM[COMP_1]*SURFACE_AREA[COMP_1]
ABSORPTION 2(t) = ABSORPTION_2(t - dt) + (FLUX_2) * dt
       INIT ABSORPTION_2 = 0
        INFLOWS:

⇒ FLUX_2 = 
              CONCENTRATIONS[COMP_2]*ADJ_PERM[COMP_2]*SURFACE_AREA[COMP_2]
   ABSORPTION_3(t) = ABSORPTION_3(t - dt) + (FLUX_3) * dt
        INIT ABSORPTION 3 = 0
        INFLOWS:
          → FLUX_3 =
              CONCENTRATIONS[COMP_3]*ADJ_PERM[COMP_3]*SURFACE_AREA[COMP_3]
   ABSORPTION 4(t) = ABSORPTION_4(t - dt) + (FLUX_4) * dt
        INIT ABSORPTION 4 = 0
        INFLOWS:
```

```
⇒ FLUX_4 =
            CONCENTRATIONS[COMP_4]*ADJ PERM[COMP 4]*SURFACE_AREA[COMP 4]
     ABSORPTION_5(t) = ABSORPTION_5(t - dt) + (FLUX 5) * dt
      INIT ABSORPTION_5 = 0
       INFLOWS:

⇒ FLUX_5 = if time<32 then
</p>
            CONCENTRATIONS[COMP_5]*ADJ_PERM[COMP_5]*SURFACE_AREA[COMP_5]*(32-ti
            me)/48*(VOL_5/17.2) else 0
     C_REL_1(t) = C_REL_1(t - dt) + (- CR_OUT_1 - CR_INPUT_1) * dt
      INIT C REL 1 = CR DOSE
       OUTFLOWS:

☆ CR_OUT_1 = IF TIME >= CUMU_TT[COMP_1] THEN C_REL_1*10000 ELSE 0

         쑹 CR_INPUT_1 = if TIME>CUMU_TT[COMP_1] then 0 else CR_RATE
   C_REL_2(t) = C_REL_2(t - dt) + (CR_OUT_1 - CR_OUT_2 - CR_INPUT_2) * dt
      INIT C REL 2 = 0
       INFLOWS:

☆ CR_OUT_1 = IF TIME >= CUMU_TT[COMP_1] THEN C_REL_1*10000 ELSE 0

Ţ
       OUTFLOWS:
I

☆ CR_OUT_2 = IF TIME >= CUMU_TT[COMP_2] THEN C_REL_2*10000 ELSE 0

ũ

☆ CR_INPUT_2 = if TIME>CUMU_TT[COMP_2] then 0 else CR_RATE

I
C_REL_3(t) = C_REL_3(t - dt) + (CR_OUT_2 - CR_OUT_3 - CR_INPUT_3) * dt
      INIT C REL 3 = 0
لللة
       INFLOWS:
Li

☆ CR_OUT_2 = IF TIME >= CUMU_TT[COMP_2] THEN C_REL_2*10000 ELSE 0

<u>L</u>
       OUTFLOWS:

☆ CR_OUT_3 = IF TIME >= CUMU_TT[COMP_3] THEN C_REL_3*10000 ELSE 0

شيق
Πij
         ★ CR_INPUT_3 = if TIME > CUMU_TT[COMP_3] then 0 else CR_RATE
1
      C_REL_4(t) = C_REL_4(t - dt) + (CR_OUT_3 - CR_OUT_4 - CR_INPUT_4) * dt
       INIT C_REL_4 = 0
Ļå
       INFLOWS:

→ CR_OUT_3 = IF TIME >= CUMU_TT[COMP_3] THEN C_REL_3*10000 ELSE 0.

       OUTFLOWS:
         ☆ CR_OUT_4 = IF TIME >= CUMU_TT[COMP_4] THEN C_REL_4*10000 ELSE 0

→ CR_INPUT_4 = if TIME>CUMU_TT[COMP_4] then 0 else CR_RATE

   C_REL_5(t) = C_REL_5(t - dt) + (CR_OUT_4 - CR_OUT_5 - CR_INPUT_5) * dt
       INIT C_REL_5 = 0
       INFLOWS:
         ★ CR_OUT_4 = IF TIME >= CUMU_TT[COMP_4] THEN C_REL_4*10000 ELSE 0
        OUTFLOWS:
         CR_OUT_5 = IF TIME >= CUMU_TT[COMP_5] THEN C_REL_5*10000 ELSE 0

☆ CR_INPUT_5 = if TIME>CUMU_TT[COMP_5] then 0 else CR_RATE

   \square C_REL_6(t) = C_REL_6(t - dt) + (CR_OUT_5) * dt
       INIT C REL 6 = 0
       INFLOWS:

★ CR_OUT_5 = IF TIME >= CUMU_TT[COMP_5] THEN C_REL_5*10000 ELSE 0
```

```
MASS_1(t) = MASS_1(t - dt) + (CR_INPUT_1 - MASS_OUT_1 - DISS_PRECIP_1) * dt
    INIT MASS_1 = DOSE
    INFLOWS:

☆ CR_INPUT_1 = if TIME>CUMU_TT[COMP_1] then 0 else CR_RATE

     OUTFLOWS:

★ MASS_OUT_1 = MASS_1*TRANSFERS[COMP 1]

      ಈ DISS_PRECIP_1 = ADJ_DISS_PRECIP[COMP_1]
MASS_2(t) = MASS_2(t - dt) + (MASS_OUT_1 + CR_INPUT_2 - MASS_OUT_2 -
    DISS_PRECIP_2) * dt
    INIT MASS 2 = 0
    INFLOWS:
      MASS_OUT_1 = MASS_1*TRANSFERS[COMP_1]
      ☆ CR_INPUT_2 = if TIME>CUMU_TT[COMP_2] then 0 else CR_RATE
    OUTFLOWS:
      * MASS_OUT_2 = MASS_2*TRANSFERS[COMP 2]
      ⇒ DISS_PRECIP_2 = ADJ_DISS_PRECIP[COMP 2]
MASS_3(t) = MASS_3(t - dt) + (CR_INPUT_3 + MASS_OUT_2 - MASS_OUT_3 -
    DISS_PRECIP_3) * dt
    INIT MASS_3 = 0
    INFLOWS:
      ★ CR_INPUT_3 = if TIME > CUMU_TT[COMP_3] then 0 else CR_RATE
      MASS_OUT_2 = MASS_2*TRANSFERS[COMP_2]
    OUTFLOWS:

★ MASS_OUT_3 = MASS_3*TRANSFERS[COMP_3]

      DISS_PRECIP_3 = ADJ_DISS_PRECIP[COMP 3]
MASS_4(t) = MASS_4(t - dt) + (CR_INPUT_4 + MASS_OUT_3 - MASS_OUT_4 -
   DISS_PRECIP_4) * dt
   INIT MASS_4 = 0
    INFLOWS:
      ★ CR_INPUT_4 = if TIME>CUMU_TT[COMP_4] then 0 else CR_RATE
      * MASS_OUT_3 = MASS_3*TRANSFERS[COMP 3]
    OUTFLOWS:
      * MASS_OUT_4 = MASS_4*TRANSFERS[COMP_4]
      DISS_PRECIP_4 = ADJ_DISS_PRECIP[COMP_4]
MASS_5(t) = MASS_5(t - dt) + (CR_INPUT_5 + MASS_OUT_4 - MASS_OUT_5 -
   DISS_PRECIP_5) * dt
   INIT MASS_5 = 0
    INFLOWS:
      ☆ CR_INPUT_5 = if TIME>CUMU_TT[COMP_5] then 0 else CR_RATE
      MASS_OUT_4 = MASS_4*TRANSFERS[COMP_4]
    OUTFLOWS:

☆ MASS_OUT_5 = if time>4 then MASS_5*TRANSFERS[COMP_5] else 0

      ⇒ DISS_PRECIP_5 = ADJ_DISS_PRECIP[COMP_5]
\square MASS_6(t) = MASS_6(t - dt) + (MASS_OUT_5) * dt
   INIT MASS 6 = 0
    INFLOWS:
```

```
★ MASS_OUT_5 = if time>4 then MASS_5*TRANSFERS[COMP_5] else 0
   SOL_1(t) = SOL_1(t - dt) + (DISS_PRECIP_1 - SOL_OUT_1 - FLUX_1) * dt
      INIT SOL 1 = 0
       INFLOWS:

⇒ DISS_PRECIP_1 = ADJ_DISS_PRECIP[COMP_1]

       OUTFLOWS:

⇒ SOL_OUT_1 = SOL_1*TRANSFERS[COMP_1]

→ FLUX_1 = 
            CONCENTRATIONS[COMP_1]*ADJ_PERM[COMP_1]*SURFACE_AREA[COMP_1]
   SOL_2(t) = SOL_2(t - dt) + (SOL_OUT_1 + DISS_PRECIP_2 - SOL_OUT_2 - FLUX_2) * dt
      INIT SOL 2 = 0
       INFLOWS:

⇒ SOL_OUT_1 = SOL_1*TRANSFERS[COMP_1]

⇒ DISS_PRECIP_2 = ADJ_DISS_PRECIP[COMP_2]

       OUTFLOWS:

⇒ SOL_OUT_2 = SOL_2*TRANSFERS[COMP_2]

I

★ FLUX_2 = 
I
            CONCENTRATIONS[COMP_2]*ADJ_PERM[COMP_2]*SURFACE_AREA[COMP_2]
Ö
Z.
    \Rightarrow SOL_3(t) = SOL_3(t - dt) + (DISS_PRECIP_3 + SOL_OUT_2 - SOL_OUT_3 - FLUX_3) * dt
U
       INIT SOL 3 = 0
Ш
       INFLOWS:

⇒ DISS_PRECIP_3 = ADJ_DISS_PRECIP[COMP_3]

         ⇒ SOL_OUT_2 = SOL_2*TRANSFERS[COMP_2]
       OUTFLOWS:
Tų.
         SOL_OUT_3 = SOL_3*TRANSFERS[COMP_3]

→ FLUX_3 = 
             CONCENTRATIONS[COMP_3]*ADJ_PERM[COMP_3]*SURFACE_AREA[COMP_3]
   = SOL 4(t) = SOL 4(t - dt) + (DISS_PRECIP_4 + SOL_OUT_3 - SOL_OUT_4 - FLUX_4) * dt
       INIT SOL 4 = 0
        INFLOWS:

⇒ DISS_PRECIP_4 = ADJ_DISS_PRECIP[COMP_4]

          SOL_OUT_3 = SOL_3*TRANSFERS[COMP_3]
        OUTFLOWS:
         SOL_OUT_4 = SOL_4*TRANSFERS[COMP_4]
         → FLUX 4 =
             CONCENTRATIONS[COMP_4]*ADJ_PERM[COMP_4]*SURFACE_AREA[COMP_4]
   \square SOL_5(t) = SOL_5(t - dt) + (DISS_PRECIP_5 + SOL_OUT_4 - SOL_OUT_5 - FLUX_5) * dt
       INIT SOL 5 = 0
        INFLOWS:
```

```
⇒ DISS_PRECIP_5 = ADJ_DISS_PRECIP[COMP_5]

⇔ SOL OUT 4 = SOL 4*TRANSFERS[COMP 4]

      OUTFLOWS:
        ⇒ SOL_OUT_5 = if time>4 then SOL_5*TRANSFERS[COMP 5] else 0

⇒ FLUX 5 = if time<32 then
</p>
           CONCENTRATIONS[COMP 5]*ADJ_PERM[COMP_5]*SURFACE AREA[COMP 5]*(32-ti
           me)/48*(VOL_5/17.2) else 0
  \bigcirc SOL_6(t) = SOL_6(t - dt) + (SOL_OUT_5) * dt
      INIT SOL 6 = 0
      INFLOWS:

⇔ SOL_OUT_5 = if time>4 then SOL_5*TRANSFERS[COMP_5] else 0

  \bigcirc VOL_1(t) = VOL_1(t - dt) + (- REABS_1 - VOL_OUT_1) * dt
      INIT VOL 1 = INIT VOLUME
      OUTFLOWS:
        REABS_1 = VOL_1*VOL_PARM[COMP_1]

★ VOL_OUT_1 = VOL_1*TRANSFERS[COMP_1]

  \bigcirc VOL_2(t) = VOL_2(t - dt) + (VOL_OUT_1 - VOL_OUT_2 - REABS_2) * dt
      INIT VOL 2 = 0
INFLOWS:
T

→ VOL_OUT_1 = VOL_1*TRANSFERS[COMP_1]

Ø
       OUTFLOWS:
I

⇒ VOL OUT 2 = VOL 2*TRANSFERS[COMP_2]

H

⇒ REABS_2 = VOL_2*VOL_PARM[COMP_2]

VOL_3(t) = VOL_3(t - dt) + (VOL_OUT_2 - VOL_OUT_3 - REABS_3) * dt
      INIT VOL 3 = 0
      INFLOWS:

⇒ VOL OUT 2 = VOL 2*TRANSFERS[COMP 2]

T
       OUTFLOWS:

★ VOL_OUT_3 = VOL_3*TRANSFERS[COMP_3]

☆ REABS_3 = VOL_3*VOL_PARM[COMP_3]

     VOL 4(t) = VOL 4(t - dt) + (VOL OUT 3 - VOL OUT 4 - REABS_4) * dt
      INIT VOL 4 = 0
       INFLOWS:

★ VOL_OUT_3 = VOL_3*TRANSFERS[COMP_3]

       OUTFLOWS:

★ VOL_OUT_4 = VOL_4*TRANSFERS[COMP_4]

         REABS_4 = VOL_4*VOL_PARM[COMP_4]
  \bigcirc VOL_5(t) = VOL_5(t - dt) + (VOL_OUT_4 - VOL_OUT_5 - REABS_5) * dt
      INIT VOL 5 = 0
       INFLOWS:

★ VOL OUT 4 = VOL_4*TRANSFERS[COMP_4]
       OUTFLOWS:

★ VOL_OUT_5 = VOL_5*TRANSFERS[COMP_5]

         REABS_5 = VOL_5*VOL_PARM[COMP_5]
  VOL_6(t) = VOL_6(t - dt) + (VOL_OUT_5) * dt
      INIT VOL 6 = 0
```

```
INFLOWS:

→ VOL_OUT_5 = VOL_5*TRANSFERS[COMP_5]

      VOL\_ABS\_1(t) = VOL\_ABS\_1(t - dt) + (REABS\_1) * dt
       INIT VOL_ABS_1 = 0
       INFLOWS:
         REABS_1 = VOL_1*VOL_PARM[COMP_1]
   \bigvee VOL_ABS_2(t) = VOL_ABS_2(t - dt) + (REABS_2) * dt
       INIT VOL ABS 2 = 0
       INFLOWS:
         REABS_2 = VOL_2*VOL_PARM[COMP_2]
   INIT VOL_ABS_3 = 0
       INFLOWS:
         REABS_3 = VOL_3*VOL_PARM[COMP_3]
   \bigvee VOL_ABS_4(t) = VOL_ABS_4(t - dt) + (REABS_4) * dt
      INIT VOL_ABS_4 = 0
       INFLOWS:
         REABS_4 = VOL_4*VOL_PARM[COMP_4]
   Ī
      INIT VOL_ABS_5 = 0
Ū
       INFLOWS:
ű
        REABS_5 = VOL_5*VOL_PARM[COMP_5]
   MULTI DOSE CALCULATION
OUTPUT CALCULATIONS
   CR_Release(t) = CR_Release(t - dt) + (CR_cumrate) * dt
Ξ
. INIT CR_Release = 0
INFLOWS:
TL:
        CUM_DISS(t) = CUM_DISS(t - dt) + (CUMM_DISS_RATE) * dt
<u>L</u>
      INIT CUM_DISS = 0
      INFLOWS:

☆ CUMM_DISS_RATE =
           DISS_PRECIP_1+DISS_PRECIP_2+DISS_PRECIP_3+DISS_PRECIP_4+DISS_PRECIP
   ABSORBED_TOTAL = ABSORPTION_2+ABSORPTION_3+ABSORPTION_4+ABSORPTION_5
   FDp% = ABSORBED_TOTAL/DOSE*100
   FLUX_TOTAL = FLUX_2+FLUX_3+FLUX_4+FLUX_5
PARMS
   O DOSE = 1000
   INIT_VOLUME = 100
   TO PARACELLULAR = 1
     pH[COMP 1] = 1.5
     pH[COMP_2] = 5
     pH[COMP_3] = 6.5
```

 $pH[COMP_4] = 7$ 

```
Km[COMPS] = [1]
       1,
       1.
       1]
    PASS_PE[COMPS] = [0,
       1.10E-06.
       2.17E-06.
       4.06E-06.
       3.80E-06]
     RC[COMP_1] = PASS_PE[COMP_1]*0
     RC[COMP_2] = IF PASS_PE[COMP_2]>0 THEN 1 ELSE 0
     RC[COMP_3] = IF PASS_PE[COMP_3]>0 THEN 2 ELSE 0
      RC[COMP_4] = IF PASS_PE[COMP_4]>0 THEN 4 ELSE 0
      RC[COMP_5] = PASS_PE[COMP_5]*0
   RCSUM = RC[COMP_2]+RC[COMP_3]+RC[COMP_4]
REGIONAL[COMP_1] = PASS_PE[COMP_1]+RCSUM*0
      REGIONAL[COMP_2] = if RCSUM=2 then
      (EXP(-9.011926 + 2.594378 *LOGN(1/PASS_PE[COMP_2]) -0.065515
      *LOGN(1/PASS_PE[COMP_2])^2))^(-1) else
E
      if RCSUM=4 then
(EXP(-0.369414*LOGN(1/PASS_PE[COMP_4])+0.23756*LOGN(1/PASS_PE[COMP_4])^2-0.009
9719*LOGN(1/PASS_PE[COMP_4])^3))^(-1) else
      if RCSUM=6 then
0.5*(EXP( -9.011926 + 2.594378 *LOGN(1/PASS_PE[COMP_3]) -0.065515
į
      *LOGN(1/PASS_PE[COMP_3])^2))^(-1)
+0.5*(EXP( -21.009845 + 4.544238 *LOGN(1/PASS_PE[COMP_4]) -0.140815
*LOGN(1/PASS_PE[COMP_4])^2))^(-1) else
PASS_PE[COMP_2]
  REGIONAL[COMP_3] = if RCSUM=1 then
      (EXP(-3.238469 + 1.509131 *LOGN(1/PASS_PE[COMP_2]) -0.022109
      *LOGN(1/PASS_PE[COMP_2])^2))^(-1) else
      if RCSUM=4 then
      (EXP(-0.093739*LOGN(1/PASS_PE[COMP_4])+0.182344*LOGN(1/PASS_PE[COMP_4])^2-0.00
      23631*LOGN(1/PASS_PE[COMP_4])^3))^(-1) else
      if RCSUM=5 then
     0.5*(EXP( -3.238469 + 1.509131 *LOGN(1/PASS_PE[COMP_2]) -0.022109
     *LOGN(1/PASS_PE[COMP_2])^2))^(-1)
     +0.5*(EXP( -15.415683 + 3.543563 *LOGN(1/PASS_PE[COMP_4]) -0.100318
     *LOGN(1/PASS_PE[COMP_4])^2))^(-1) else
     PASS_PE[COMP_3]
```

```
REGIONAL[COMP 4] = if RCSUM=1 then
      (EXP( 14.455255 -1.264630 *LOGN(1/PASS_PE[COMP_2]) + 0.082015
      *LOGN(1/PASS_PE[COMP_2])^2))^(-1) else
      if RCSUM=2 then
      (EXP( 11.480333 -0.791109 *LOGN(1/PASS_PE[COMP_3]) + 0.066063
      *LOGN(1/PASS_PE[COMP_3])^2))^(-1) else
      if RCSUM=3 then
      0.5*(EXP( 14.455255 -1.264630 *LOGN(1/PASS_PE[COMP_2]) + 0.082015
      *LOGN(1/PASS_PE[COMP_2])^2))^(-1)
      +0.5*(EXP( 11.480333 -0.791109 *LOGN(1/PASS_PE[COMP_3]) + 0.066063
      *LOGN(1/PASS_PE[COMP_3])^2))^(-1) else
      PASS PE[COMP_4]
   REGIONAL[COMP_5] = PASS_PE[COMP_5] +RCSUM*0
SOLUBILIY CALCULATION
   ADJ_SOLUB[COMP_1] = if USER_pH[COMP_1]>=pH[COMP_1] then USER_SOLUB[COMP_1]
      ((USER SOLUB[COMP 2]-USER SOLUB[COMP 1])/(USER_pH[COMP 2]-USER pH[COMP 1]
      ))*(pH[COMP_1]-USER_pH[COMP_1])+USER_SOLUB[COMP_1]
   ADJ_SOLUB[COMP_2] = if USER_pH[COMP_2]=pH[COMP_2] then USER_SOLUB[COMP_2]
T
       eise if USER_pH[COMP_2]<pH[COMP_2] then
Ō
       ((USER_SOLUB[COMP_3]-USER_SOLUB[COMP_2])/(USER_pH[COMP_3]-USER_pH[COMP_2]
ı,
       ))*(pH[COMP_2]-USER_pH[COMP_2])+USER_SOLUB[COMP_2] else
17
       ((USER_SOLUB[COMP_2]-USER_SOLUB[COMP_1])/(USER_pH[COMP_2]-USER_pH[COMP_1]
))*(pH[COMP 2]-USER pH[COMP 1])+USER SOLUB[COMP 1]
      ADJ_SOLUB[COMP_3] = if USER_pH[COMP_3]=pH[COMP_3] then USER_SOLUB[COMP_3]
       else if USER_pH[COMP_3]<pH[COMP_3] then
1
       ((USER_SOLUB[COMP_4]-USER_SOLUB[COMP_3])/(USER_pH[COMP_4]-USER_pH[COMP_3]
       ))*(pH[COMP_3]-USER_pH[COMP_3])+USER_SOLUB[COMP_3] else
TŲ.
       ((USER_SOLUB[COMP_3]-USER_SOLUB[COMP_2])/(USER_pH[COMP_3]-USER_pH[COMP_2]
<u>.</u>
       ))*(pH[COMP 3]-USER pH[COMP_2])+USER_SOLUB[COMP_2]
ADJ_SOLUB[COMP_4] = if USER_pH[COMP_4]=pH[COMP_4] then USER_SOLUB[COMP_4]
       else if USER_pH[COMP_4]<pH[COMP_4] then
       ((USER_SOLUB[COMP_5]-USER_SOLUB[COMP_4])/(USER_pH[COMP_5]-USER_pH[COMP_4]
       ))*(pH(COMP 4)-USER pH(COMP 4))+USER SOLUB[COMP_4] else
       ((USER_SOLUB[COMP_4]-USER_SOLUB[COMP_3])/(USER_pH[COMP_4]-USER_pH[COMP_3])
       ))*(pH[COMP_4]-USER_pH[COMP_3])+USER_SOLUB[COMP_3]
   ADJ_SOLUB[COMP_5] = if USER_pH[COMP_3]=pH[COMP_3] then USER_SOLUB[COMP_3]
       else if USER_pH[COMP_3]<pH[COMP_3] then
       ((USER_SOLUB[COMP_4]-USER_SOLUB[COMP_3])/(USER_pH[COMP_4]-USER_pH[COMP_3]
       ))*(pH[COMP_3]-USER_pH[COMP_3])+USER_SOLUB[COMP_3] else
       ((USER_SOLUB[COMP_3]-USER_SOLUB[COMP_2])/(USER_pH[COMP_3]-USER_pH[COMP_2]
       ))*(pH[COMP_3]-USER_pH[COMP_2])+USER_SOLUB[COMP_2]
    USER_pH[COMPS] = [1.5 ,
       5,
       6.5,
       7,
       7.5]
```

```
USER_SOLUB[COMPS] = [31,
      3.65 .
      3.65,
      3.65,
      3.65]
TRANSIT TIME
      ADJ_TRANSIT_TIME[COMP_1] = .5*TRANSIT_ADJ[COMP_1]*USER_TT_INPUT
      ADJ TRANSIT_TIME[COMP_2] = .25*TRANSIT_ADJ[COMP_2]*USER_TT_INPUT
      ADJ_TRANSIT_TIME[COMP_3] = 1.5°TRANSIT_ADJ[COMP_3]*USER_TT_INPUT
      ADJ TRANSIT TIME[COMP 4] = 1.5*TRANSIT ADJ[COMP 4]*USER TT INPUT
      ADJ TRANSIT_TIME[COMP_5] = 24°TRANSIT_ADJ[COMP_5]°USER_TT_INPUT
      CUMU TTICOMP 1] = ADJ TRANSIT TIME[COMP 1]
      CUMU_TT[COMP_2] = ADJ_TRANSIT_TIME[COMP_1]+ADJ_TRANSIT_TIME[COMP_2]
CUMU TT[COMP 3] =
      ADJ_TRANSIT_TIME[COMP_1]+ADJ_TRANSIT_TIME[COMP_2]+ADJ_TRANSIT_TIME[COMP_
   CUMU_TT[COMP_4] =
      ADJ_TRANSIT_TIME[COMP_1]+ADJ_TRANSIT_TIME[COMP_2]+ADJ_TRANSIT_TIME[COMP_
Tring.
      3]+ADJ_TRANSIT_TIME[COMP_4]
   O CUMU_TT[COMP_5] =
      ADJ TRANSIT TIME[COMP 1]+ADJ TRANSIT TIME[COMP 2]+ADJ TRANSIT TIME[COMP
      3)+ADJ TRANSIT_TIME[COMP_4]+ADJ_TRANSIT_TIME[COMP_5]
TRANSFERS[COMP_1] = LOGN(10)ADJ_TRANSIT_TIME[COMP_1]
      TRANSFERS[COMP_2] = LOGN(10)ADJ_TRANSIT_TIME[COMP_2]
      TRANSFERS[COMP_3] = LOGN(10)ADJ_TRANSIT_TIME[COMP_3]
       TRANSFERS[COMP_4] = LOGN(10)ADJ_TRANSIT_TIME[COMP_4]
       TRANSFERS[COMP_5] = LOGN(10)ADJ_TRANSIT_TIME[COMP_5]
       USER_TT_INPUT = 1
```

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